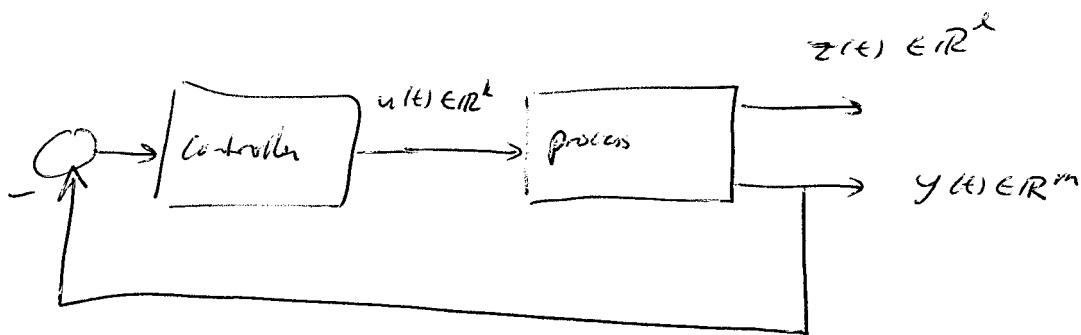


Lecture 20 LQR



process :

$$\dot{x} = Ax + Bu \quad \leftarrow \text{state equation}$$

$$y = Cx \quad \leftarrow \text{output or measured output (from sensors)}$$

$$z = Gx + Hu \quad \leftarrow \text{controlled output - things you want to make small}$$

Example : to make y small let

$$G = C \quad \text{and} \quad H = 0$$

$$\Rightarrow z = Cx = y$$

Example : to make $\begin{pmatrix} y \\ \dot{y} \end{pmatrix}$ small, let

$$z = \begin{pmatrix} y \\ \dot{y} \end{pmatrix} = \begin{pmatrix} Cx \\ C\dot{x} \end{pmatrix} = \begin{pmatrix} Cx \\ CAx + CBu \end{pmatrix} = \underbrace{\begin{pmatrix} C \\ CA \end{pmatrix}}_G x + \underbrace{\begin{pmatrix} 0 \\ CB \end{pmatrix}}_H u$$

20.2 Optimal Regulation

LQR optimality criteria:

$$J_{LQR} = \underbrace{\int_0^{\infty} \|z(t)\|^2 dt}_{\text{energy of controlled output}} + \underbrace{\rho \int_0^{\infty} \|u(t)\|^2 dt}_{\text{energy of controlled input}} \quad \rho > 0$$

ρ - large implies $\int_0^{\infty} \|u(t)\|^2 dt$ small at the expense of $\int_0^{\infty} \|z(t)\|^2 dt$

ρ - small - $\int_0^{\infty} \|z(t)\|^2 dt$ small at the expense of large input

More generally we have

$$J_{LQR} = \int_0^{\infty} z^T \bar{Q} z + \rho u^T \bar{R} u dt$$

Since $z = Gx + Hu$ we get

$$\begin{aligned} J_{LQR} &= \int_0^{\infty} (Gx + Hu)^T \bar{Q} (Gx + Hu) + \rho u^T \bar{R} u dt \\ &= \int_0^{\infty} x^T G^T \bar{Q} G x + u^T (\rho \bar{R} + H^T \bar{Q} H) u + 2 x^T G^T \bar{Q} H u dt \end{aligned}$$

Letting $Q \triangleq G^T \bar{Q} G$, $R \triangleq \rho \bar{R} + H^T \bar{Q} H$, $N \triangleq G^T \bar{Q} H$

$$J_{LQR} = \int_0^{\infty} x^T Q x + u^T R u + 2 x^T N u dt$$

20.3 Feedback Invariants

Recall: Given $\dot{x} = Ax + Bu$ $x(0) = x_0$ (3.1)

$H(x(t), u(t))$ is a feedback invariant if it only depends on x_0 and not $u(t), t \geq 0$

Proposition 20.1

If $\lim_{t \rightarrow \infty} x(t) = 0$ then for every symmetric P ,

$$H(x(t), u(t)) = - \int_0^{\infty} (Ax + Bu)^T P x + x^T P (Ax + Bu) dt \quad (3.2)$$

is a feedback invariant

proof:

$$\begin{aligned}
 H(x(t), u(t)) &= - \int_0^{\infty} \frac{d}{dt} (x^T(t) P x(t)) dt \\
 &= - \lim_{t \rightarrow \infty} x^T(t) P x(t) + x_0^T P x_0 \\
 &= x_0^T P x_0
 \end{aligned}$$

20.4

q

$$J = H(x(t), u(t)) + \int_0^{\infty} L(x(t), u(t)) dt$$

where H is a feedback invariant and $L(x, u)$ satisfies

$$\min_{u \in \mathbb{R}^k} L(x, u) = 0$$

then the control that minimizes J is

$$u^*(t) = \operatorname{arg\,min}_{u \in \mathbb{R}^k} L(x(t), u)$$

and $J^* = H(x(\cdot), u(\cdot))$

20.5 Optimal State Feedback

$$J_{LQR} = \int_0^{\infty} x^T Q x + u^T R u + 2 x^T N u dt$$

The idea is to add and subtract ^{the} a feedback invariant (3.2)

$$J_{LQR} = H(x(t), u(t)) + \int_0^{\infty} [x^T Q x + u^T R u + 2 x^T N u + (A + B u)^T P x + x^T P (A + B u)] dt$$

$$= H(x(t), u(t)) + \int_0^{\infty} [x^T (A^T P + P A + Q) x + u^T R u + 2 u^T (B^T P + N^T) x] dt$$

complete the squares

$$\begin{aligned} (u + kx)^T R (u + kx) &= u^T R u + u^T R k x + x^T k^T R u + x^T k^T R k x \\ &= u^T R u + 2 u^T R k x + x^T k^T R k x \end{aligned}$$

comparing terms, let $Rk = B^T P + N^T$

$$\Rightarrow k = R^{-1} (B^T P + N^T)$$

$$J_{LQR} = H(x(t), u(t)) + \int_0^{\infty} \left[(u + kx)^T R (u + kx) + x^T (A^T P + PA + Q - K^T R K) x \right] dt \tag{5.1}$$

Since $H(x(t), u(t))$ is a quadratic invariant for any symmetric P , ~~select~~ select P as the symmetric solution of

$$A^T P + PA + Q - K^T R K = 0 \tag{5.2}$$

to get

$$J_{LQR} = H(x(t), u(t)) + \int_0^{\infty} (u + kx)^T R (u + kx) dt$$

Note that if $R > 0$ then

$$\min_{w \in \mathbb{R}^k} (w + kx)^T R (w + kx) = 0$$

and

$$u^*(t) = \arg \min_{w \in \mathbb{R}^k} (w + kx)^T R (w + kx) = -K x(t)$$

or $u^*(t) = -R^{-1} (B^T P + N^T) x(t)$ (5.3)

Eq (5.2) becomes

$$A^T P + PA + Q - (R^{-1} (B^T P + N^T))^T R (R^{-1} (B^T P + N^T)) = 0$$

$$\Leftrightarrow \boxed{A^T P + PA + Q - (PB + N) R^{-1} (B^T P + N^T) = 0} \tag{5.4}$$

Algebraic Riccati Equation

Discrete Time

$$x_{k+1} = Ax_k + Bu_k$$

also x_0 - initial condition

$$y_k = Cx_k$$

$$z_k = Gx_k + Hu_k$$

$$J_{LQR} = \sum_{j=0}^{\infty} x_j^T Q x_j + u_j^T R u_j + 2x_j^T N u_j$$

For discrete-time systems, we need a feedback invariant

try

$$H(x(\cdot), u(\cdot)) = - \sum_{j=0}^{\infty} \{ (Ax_j + Bu_j)^T P (Ax_j + Bu_j) - x_j^T P x_j \}$$

$$= - \sum_{j=0}^{\infty} \{ x_{j+1}^T P x_{j+1} - x_j^T P x_j \}$$

$$= - \left\{ \begin{array}{l} (x_1^T P x_1 - x_0^T P x_0) \\ + (x_2^T P x_2 - x_1^T P x_1) \\ + (x_3^T P x_3 - x_2^T P x_2) \\ \dots \end{array} \right\}$$

$$= x_0^T P x_0 - \lim_{j \rightarrow \infty} x_j^T P x_j$$

\therefore If $x_j \rightarrow 0$ then $H(x(\cdot), u(\cdot))$ is a feedback invariant for any P

The next step is to write J_{LQR} in terms of H :

$$J_{LQR} = H(x(\cdot), u(\cdot)) + \sum_{j=0}^{\infty} \left\{ x_j^T Q x_j + u_j^T R u_j + 2 x_j^T N u_j - x_j^T A^T P A x_j - u_j^T B^T P B u_j - 2 u_j^T B^T P A x_j - x_j^T P x_j \right\}$$

$$= H(x(\cdot), u(\cdot)) + \sum_{j=0}^{\infty} \left\{ u_j^T (R - B^T P B) u_j + 2 u_j^T (B^T P A - N^T) x_j + x_j^T (A^T P A + P - Q) x_j \right\}$$

complete square

$$\mathcal{M} (u_j + \tilde{k} x_j)^T \bar{R} (u_j + \tilde{k} x_j) = u_j^T \bar{R} u_j + 2 u_j^T \bar{R} \tilde{k} x_j + x_j^T \tilde{k}^T \bar{R} \tilde{k} x_j$$

comparing terms, let $\bar{R} = (R - B^T P B)$

$$\text{and } \bar{R} \tilde{k} = B^T P A - N^T$$

$$\Rightarrow \boxed{K = (R - B^T P B)^{-1} (B^T P A - N^T)}$$

$$\Rightarrow J_{LQR} = H(x(\cdot), u(\cdot)) + \sum_{j=0}^{\infty} \left\{ (u_j + k x_j)^T (R - B^T P B) (u_j + k x_j) - x_j^T (A^T P A + P - Q - K^T (R - B^T P B) K) x_j \right\}$$

If we select P as the solution of

$$\boxed{A^T P A + P - Q - (A^T P B - N) (R - B^T P B)^{-1} (B^T P A - N^T) = 0}$$

then

$$J_{LQR} = H(x(\cdot), u(\cdot)) + \sum_{j=0}^{\infty} (u_j + k x_j)^T (R - B^T P B) (u_j + k x_j)$$

$$\text{if } R - B^T P B > 0 \text{ then } \boxed{u_j^* = -K x_j}$$

Bryson's Rule

For

$$J_{LQR} = \int_0^{\infty} (z^T \bar{Q} z + u^T \bar{R} u) dt$$

Bryson's rule is to select \bar{Q} and \bar{R} as diagonal matrices with

$$\bar{Q}_{ii} = \frac{1}{\text{max acceptable value of } z_i^2}$$

$$\bar{R}_{ii} = \frac{1}{\text{max acceptable value of } u_i^2}$$

Basic idea: Normalize the units.

Tune from there.